

Mechanical Performance of Large Format Underwater Photomultiplier

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BNL

6/16/2012

ProjectX@FNAL

Introduction

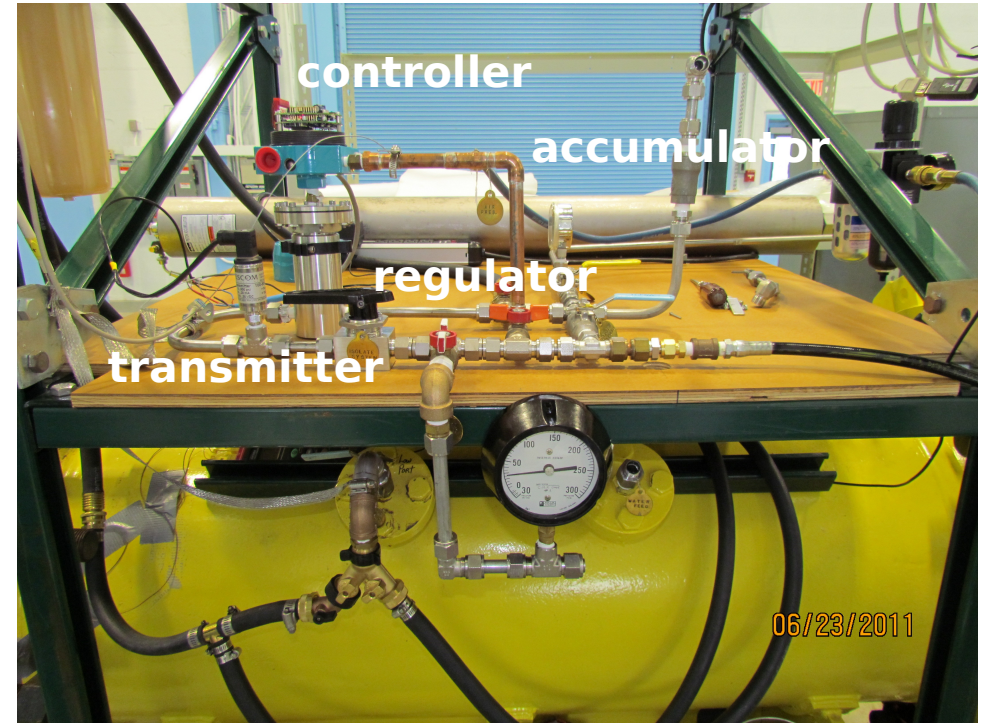
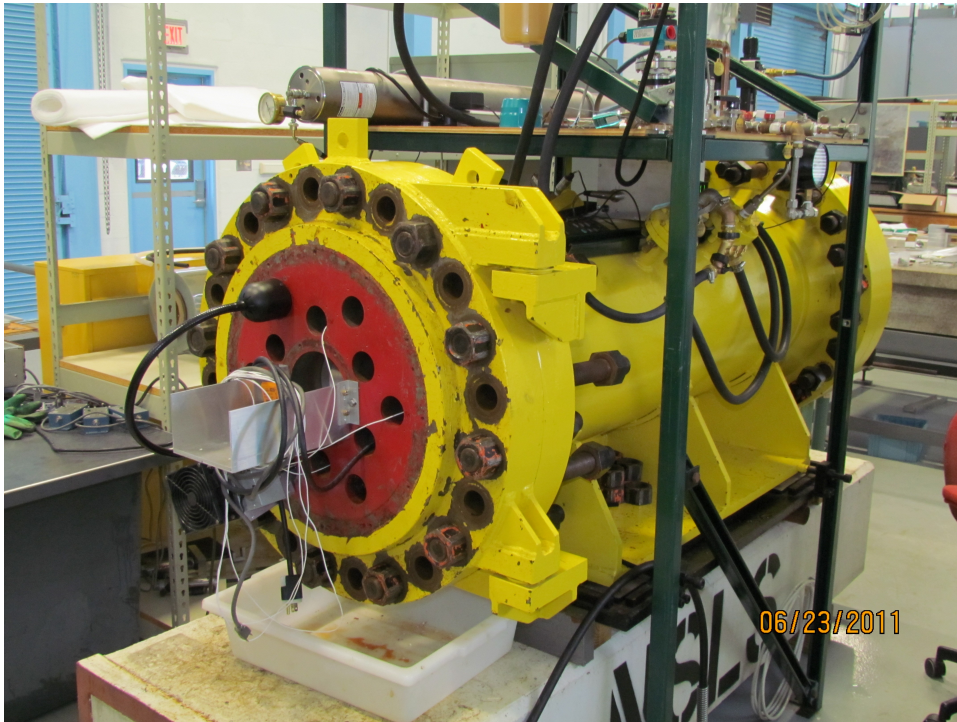
Large water Cerenkov detectors are important technology for neutrino physics from MeV to TeV energy range.

- Mechanic performance of large format semi-hemispherical photomultiplier (PMT) within large water Cerenkov detector
 - Determine if the PMT can withstand expected hydrostatic pressure and potential shock waves in the water
 - 6600 PMTs imploded in Super Kamiokande in a chain reaction by the shock wave in 2001
 - BNL hydrostatic pressure test
 - PMT underwater implosion test
 - Single PMT implosion test
 - Multiple PMTs cascade implosion test
 - PMT Implosion Simulation

Slow Rise Pressure Test

- Goal: Check the performance of glass under slow rise pressure conditions. How much strength of glass decreases (changes) if we rise the pressure slowly. This will help us to decide the correct pressure rating of PMT glass.
- Hydrostatic pressure tests:
 - Multiple different types of PMTs (10", 11" and 12") in 5 minutes / 2 hours / 24 hours cycle each (0-300psi)

BNL Slow Rise system

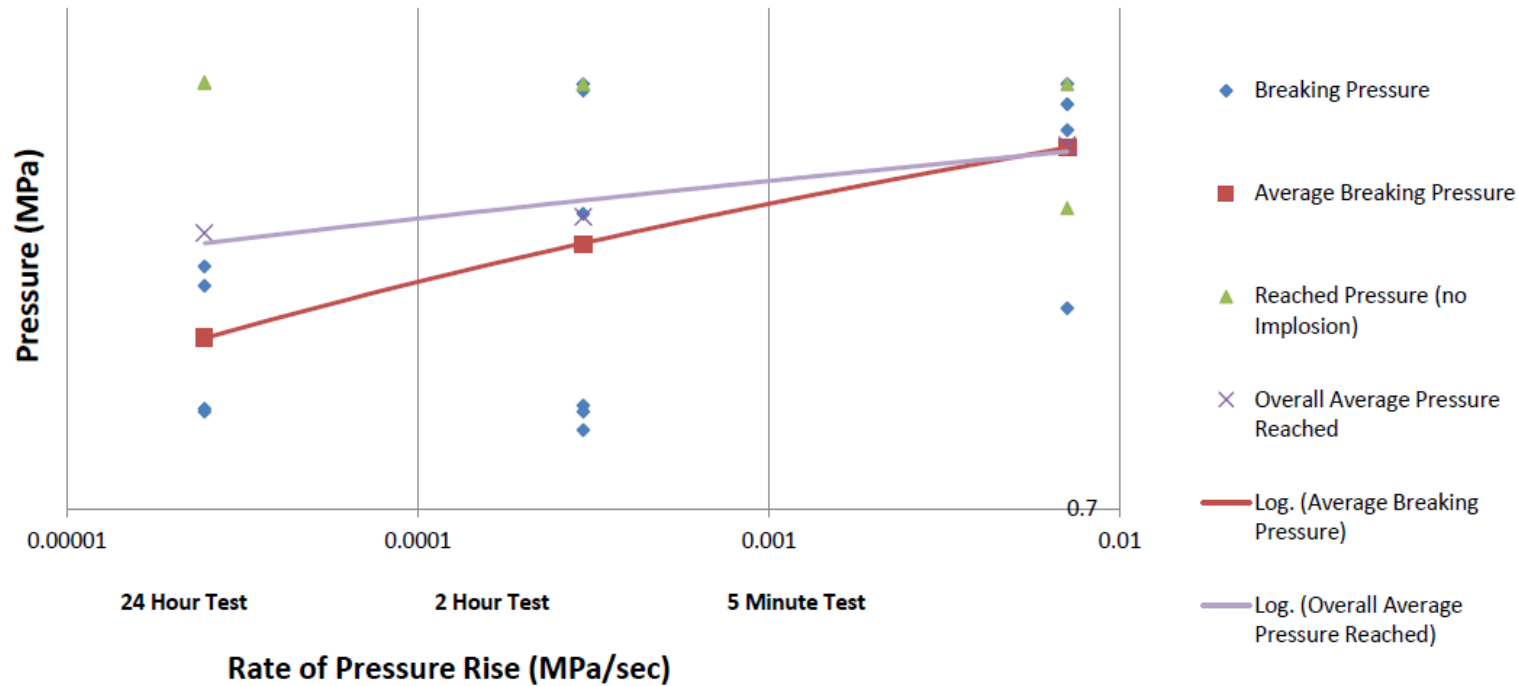


Slow rise system:

- BNL pressure vessel tank (50gal, up to 350psi)
- High pressure accumulator feed in (3gal, up to 2000 psi)
- Tap water feed in (up to 60 psi)
- Regulator / transmitter feed back
- ER3000 Electronic Pressure Controller
- Labview control the pressure rising function

10" PMTs

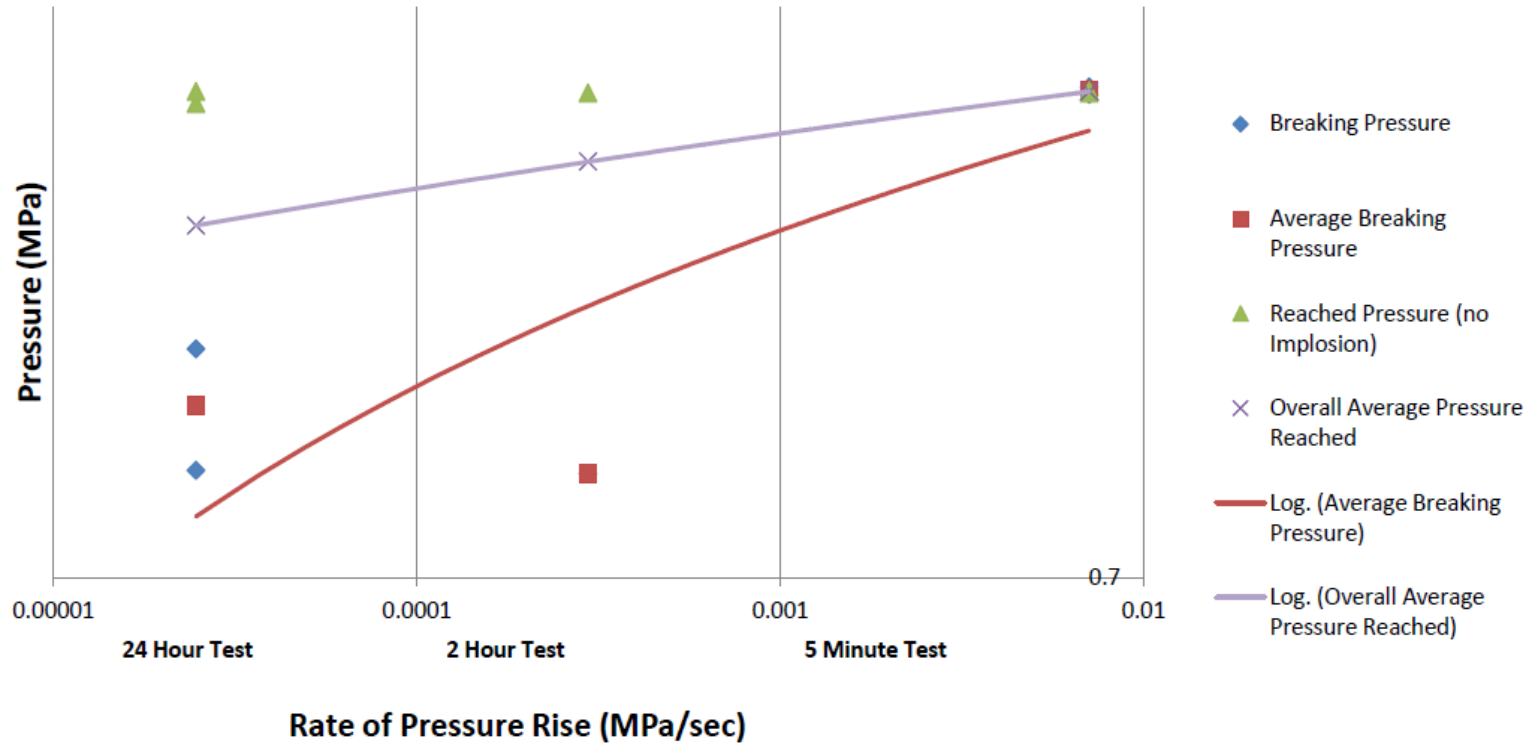
10" PMT - Pressure vs. Rate of Pressure Rise



| 10" PMTs | Rate of Pressure Rise (MPa/sec) | Breaking Pressure (MPa) | Average Breaking Pressure (MPa) | Reached Pressure (MPa) [no Implosion] | Overall Average Pressure Reached (MPa) |
|---------------|---------------------------------|-------------------------|---------------------------------|---------------------------------------|--|
| 5 Minute Test | 0.0071016 | 1.95811107 | 1.75471573 | 2.06153243 1.503057089 | 1.76390874 |
| | 0.0071016 | 1.834005439 | | | |
| | 0.0071016 | 1.165213982 | | | |
| | 0.0071016 | 2.06153243 | | | |
| 2 Hour Test | 0.00029647 | 2.06153243 | 1.372056701 | 2.06153243 | 1.470553233 |
| | 0.00029647 | 0.854949904 | | | |
| | 0.00029647 | 2.027058643 | | | |
| | 0.00029647 | 1.482372817 | | | |
| | 0.00029647 | 0.910107962 | | | |
| | 0.00029647 | 0.896318448 | | | |
| 24 Hour Test | 0.00002468 | 0.896318448 | 1.082476895 | 2.068427187 2.068427187 | 1.411126992 |
| | 0.00002468 | 1.234161555 | | | |
| | 0.00002468 | 1.296214371 | | | |
| | 0.00002468 | 0.903213205 | | | |

11" PMTs

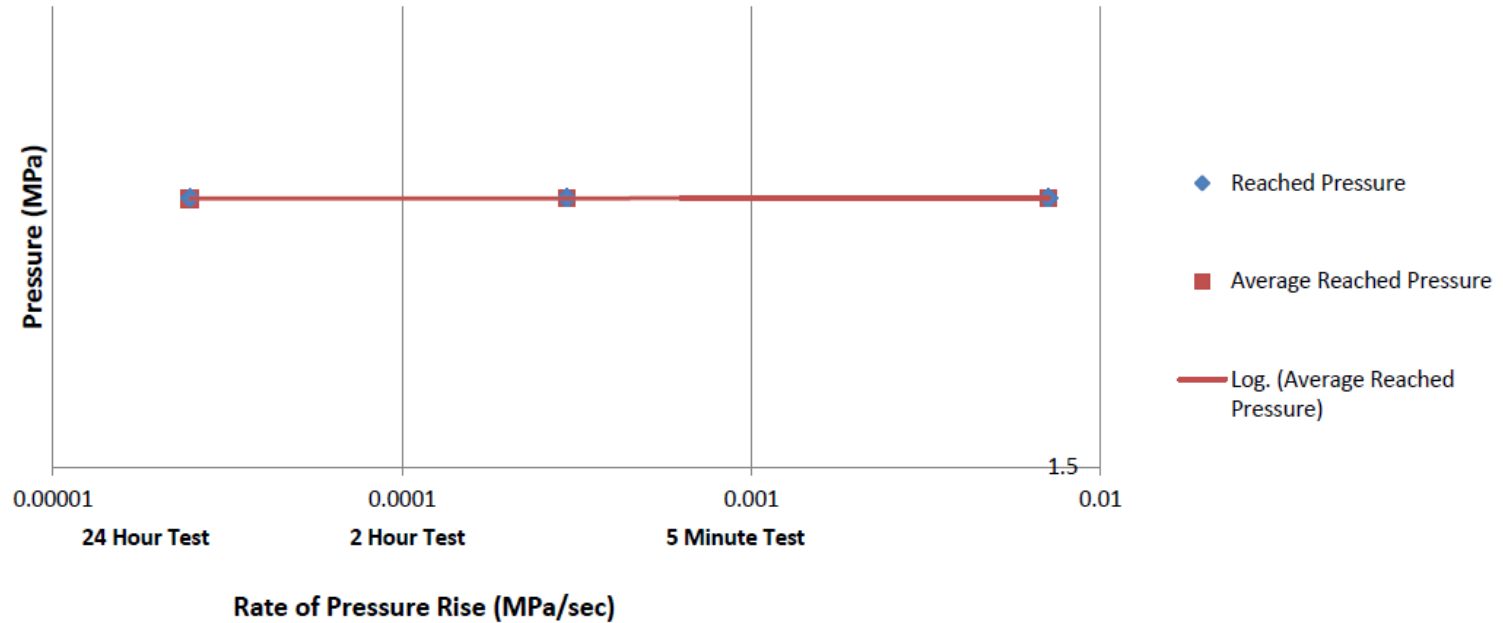
11" PMT - Pressure vs. Rate of Pressure Rise



| 11" PMTs | Rate of Pressure Rise (MPa/sec) | Breaking Pressure (MPa) | Average Breaking Pressure (MPa) | Reached Pressure (MPa) [no Implosion] | Overall Average Pressure Reached (MPa) |
|---------------|---------------------------------|-------------------------|---------------------------------|---------------------------------------|--|
| 5 Minute Test | 0.0071016 | 2.054637672 | 2.071874566 | 2.06153243 | 2.068427187 |
| | 0.0071016 | 2.089111459 | | 2.068427187 | |
| | 0.0071016 | | | 2.068427187 | |
| 2 Hour Test | 0.00029647 | 0.882528933 | 0.882528933 | 2.06153243 | 1.770228934 |
| | | | | 2.068427187 | |
| | | | | 2.068427187 | |
| 24 Hour Test | 0.00002468 | 1.165213982 | 1.027318836 | 2.013269129 | 1.534083497 |
| | 0.00002468 | 0.88942369 | | 2.068427187 | |

12" PMTs

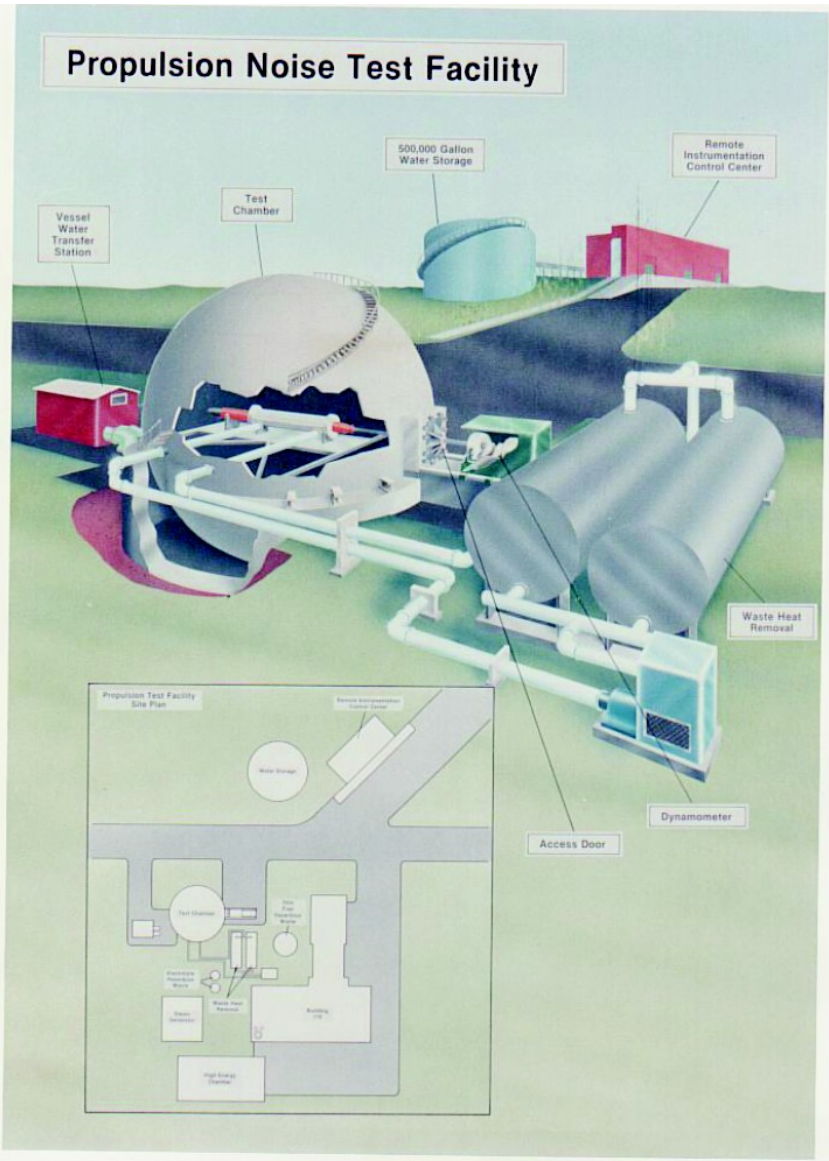
12" PMT - Pressure vs. Rate of Pressure Rise



20 PMTs for 5 mins and 2 hours tests
5 PMTs for 24 hours tests.

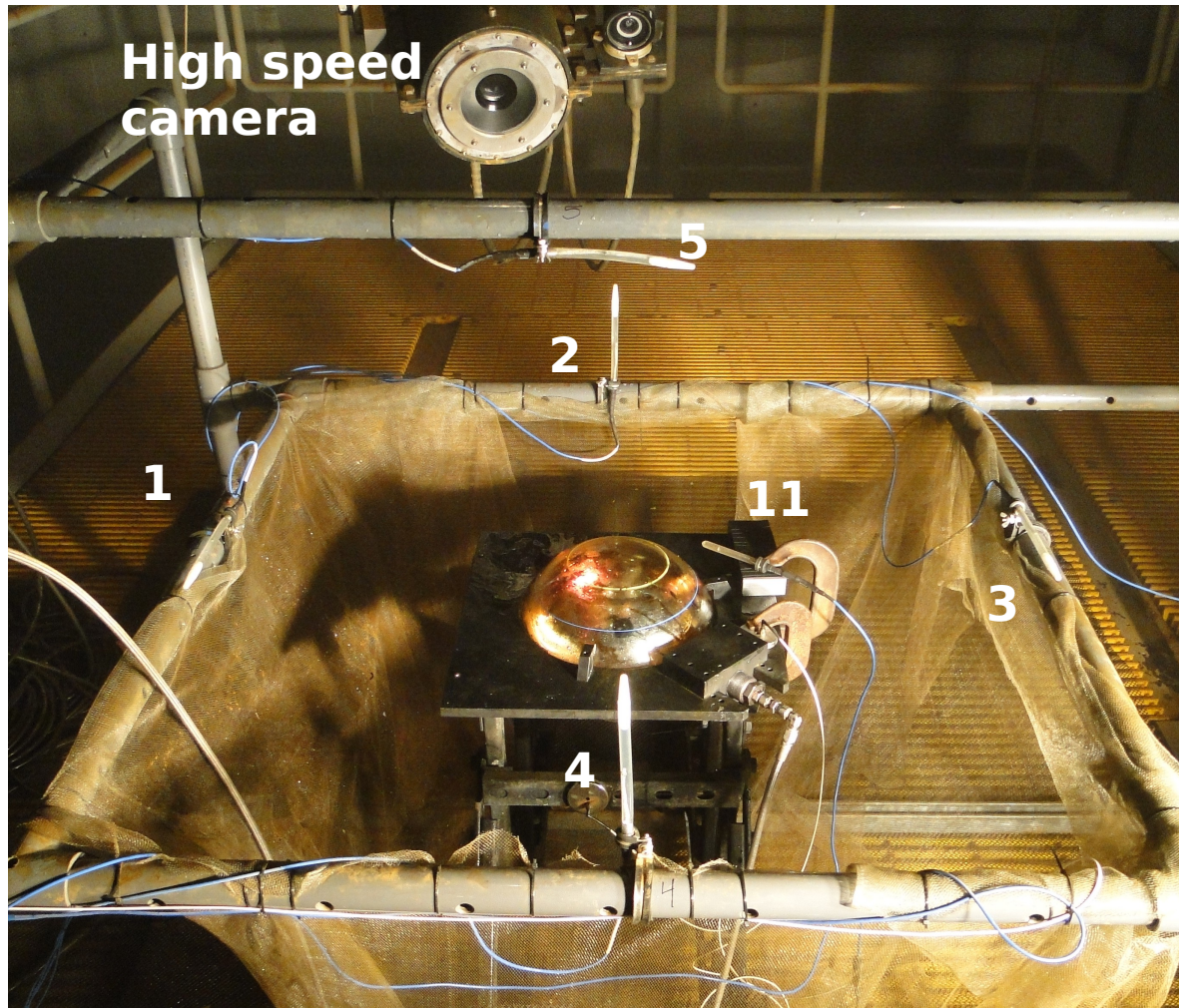
All survived.

Navy Undersea Warfare Center (NUWC) Facility

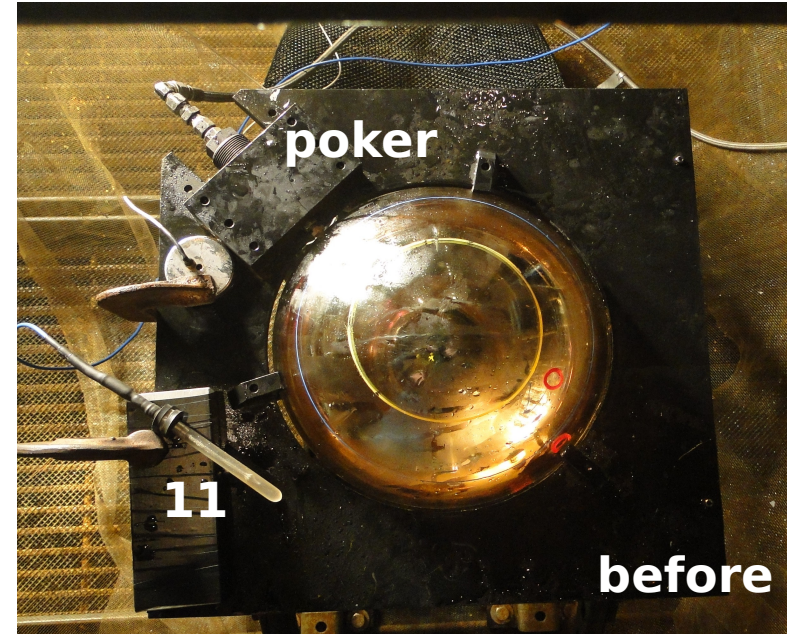


- Cooperation between BNL and NUWC through Cooperative Research And Development Agreement (CRADA)
- 15m diameter
- 500,000 gallons of water
- Rated for 100 psi at the center

Single PMT Experimental Setup



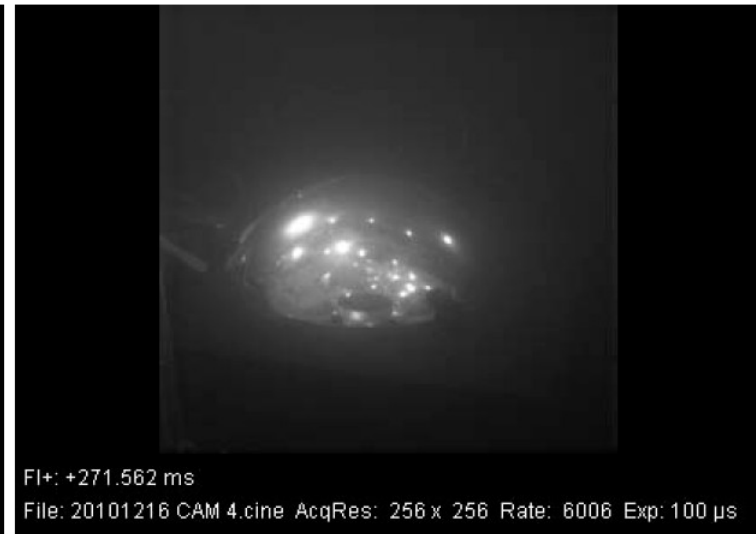
7 Water proof pressure sensors (PCB ICP)
2 High speed cameras



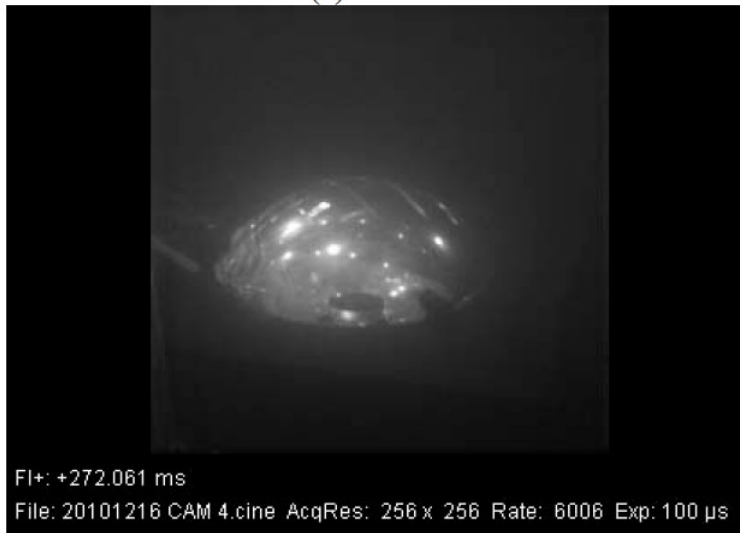
12/16/2010 Implosion Test



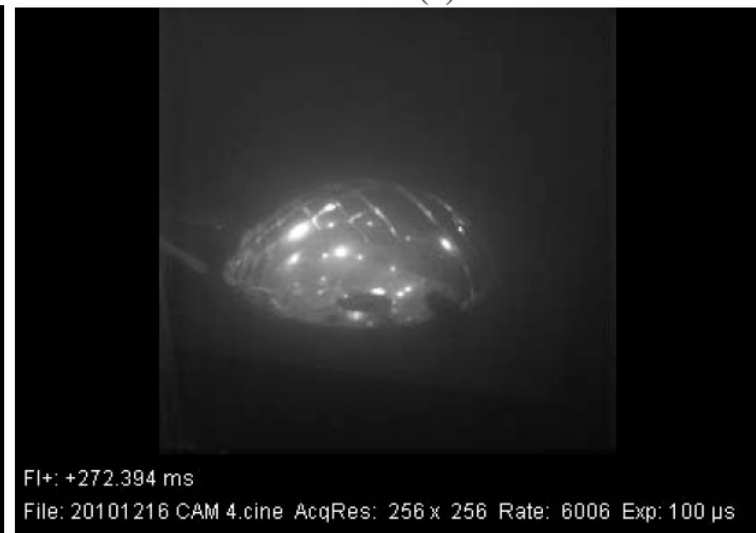
(a)



(b)

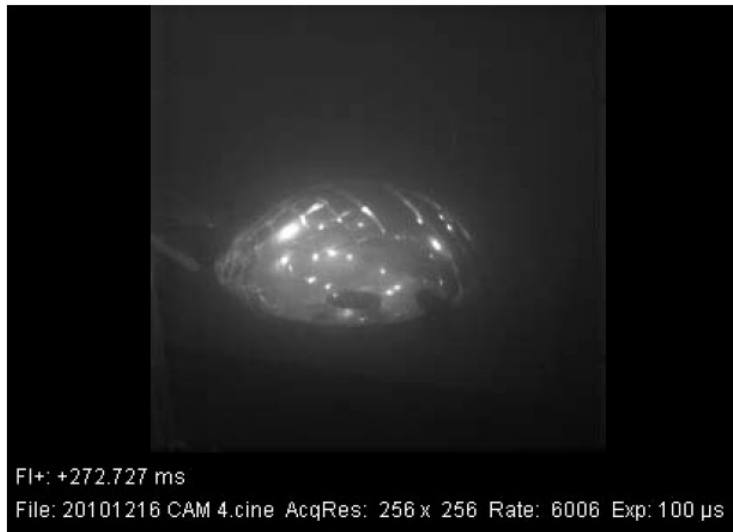


(c)

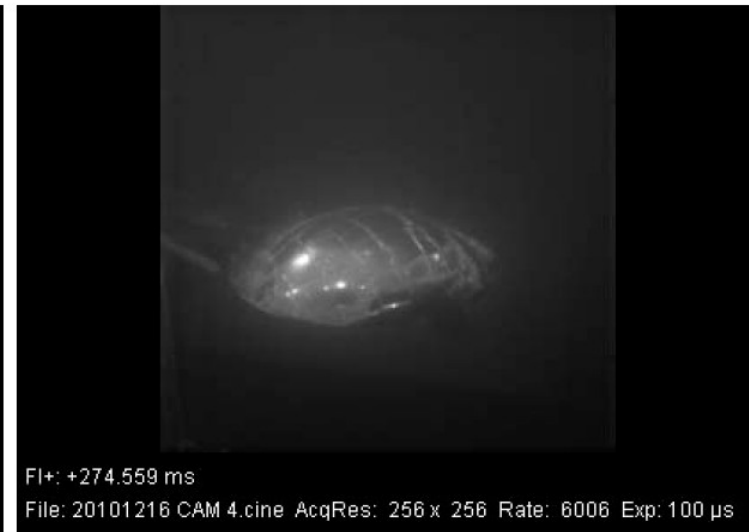


(d)

12/16/2010 Implosion Test



(e)



(f)

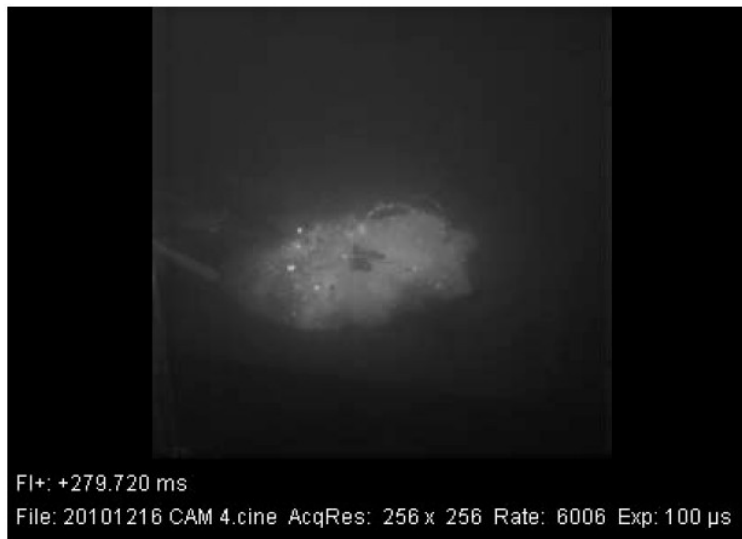


(g)



(h)

12/16/2010 Implosion Test



(i)



(j)



(k)

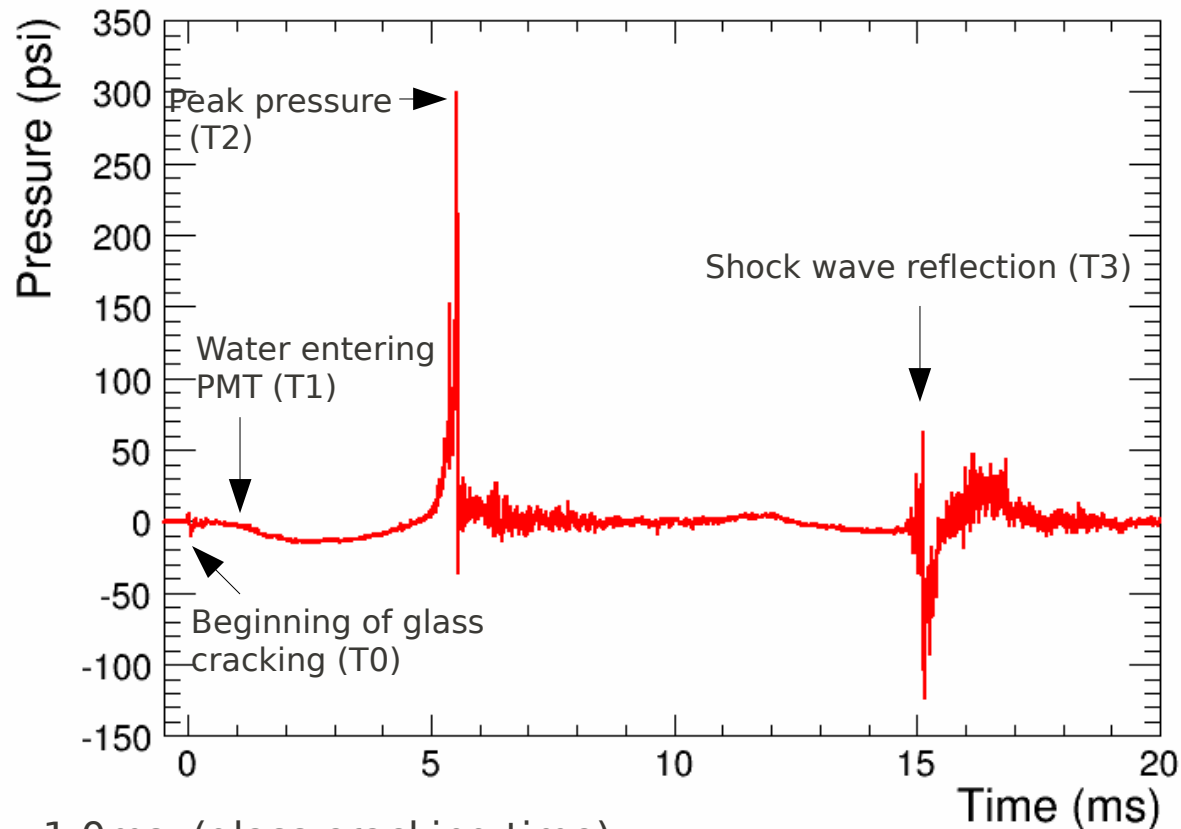


(l)

Blast Sensor Pulse Structure

Sensor ACC5 Response (500KHz)

Dec/16/2010



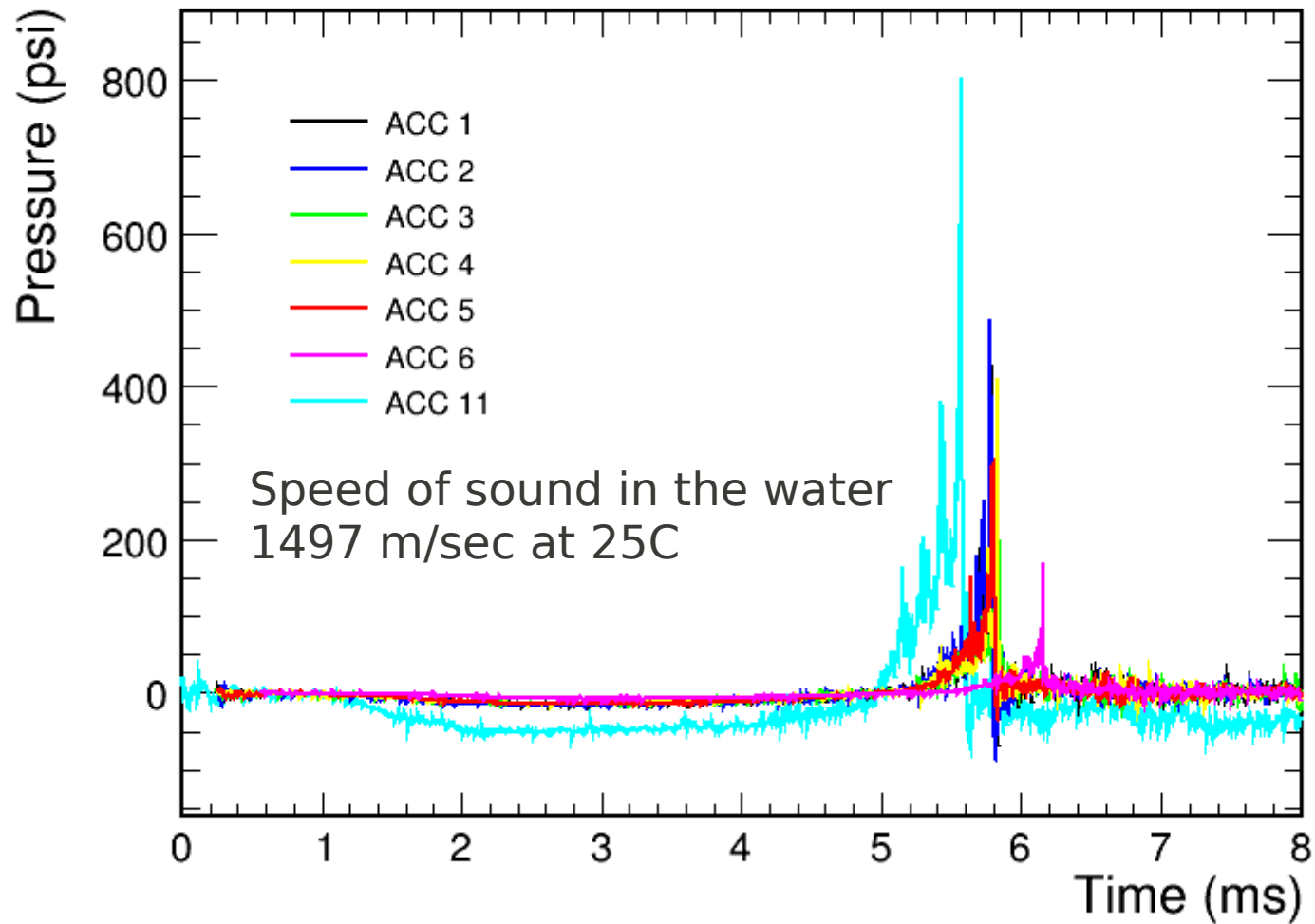
T1 - T0 ~ 1.0ms (glass cracking time)

T2 - T1 ~ 4.5ms >> 0.8ms (sound traveling time)

T3 - T2 ~ 10 ms (close to the speed of sound)

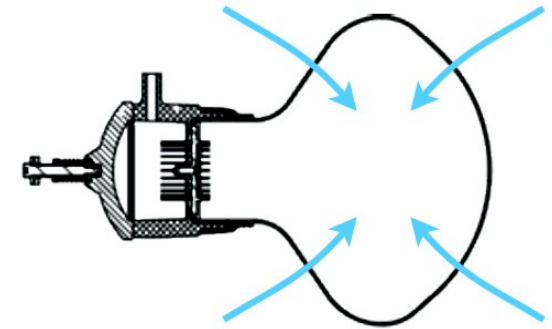
Multiple Sensors

Pressure Sensor Response [12/16/10 PMT Test]

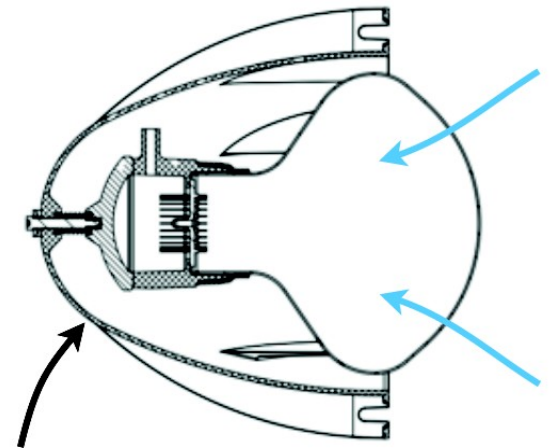


PMT with bucket

- A new design of PMT with “bucket” housing
- Expect: asymmetric flow spreads the energy out in time
 - Lower intensity of outgoing shock wave.

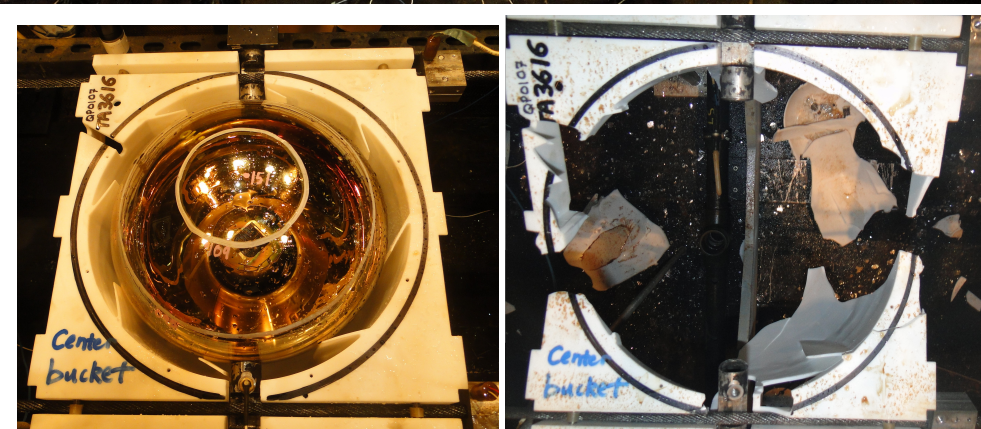
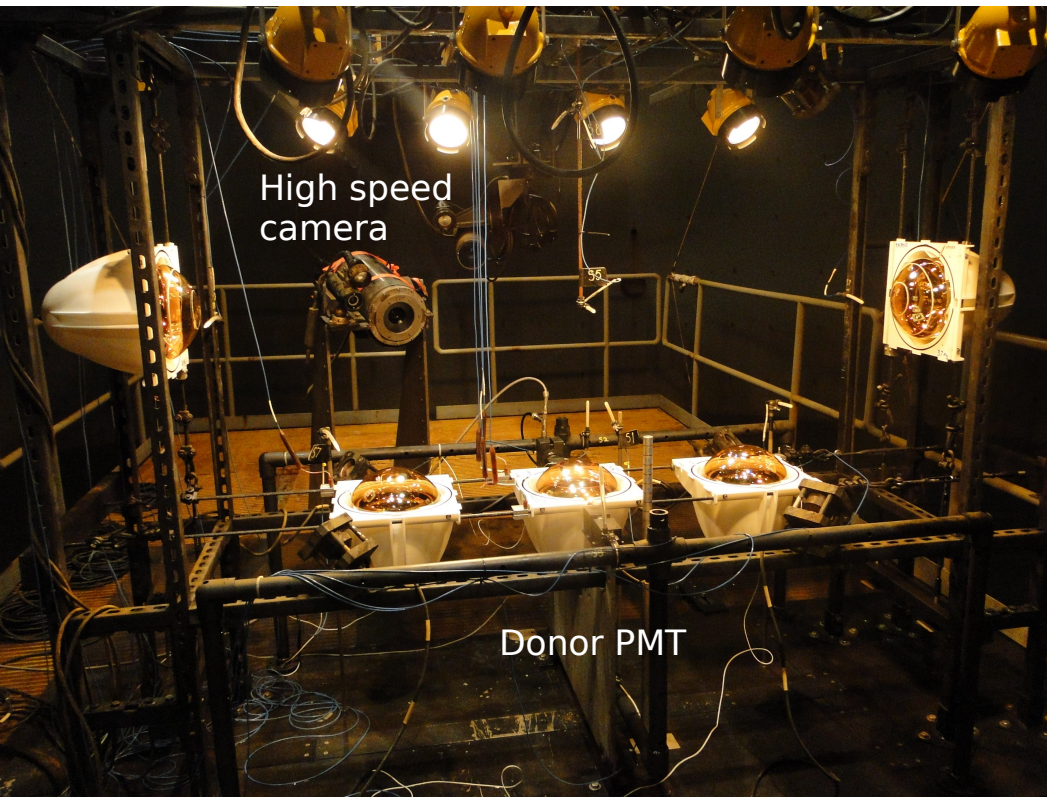


(Comparing to bare PMT)



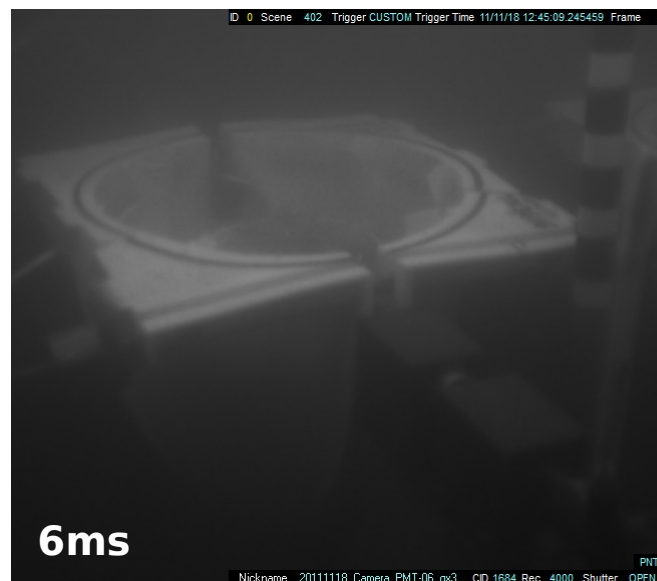
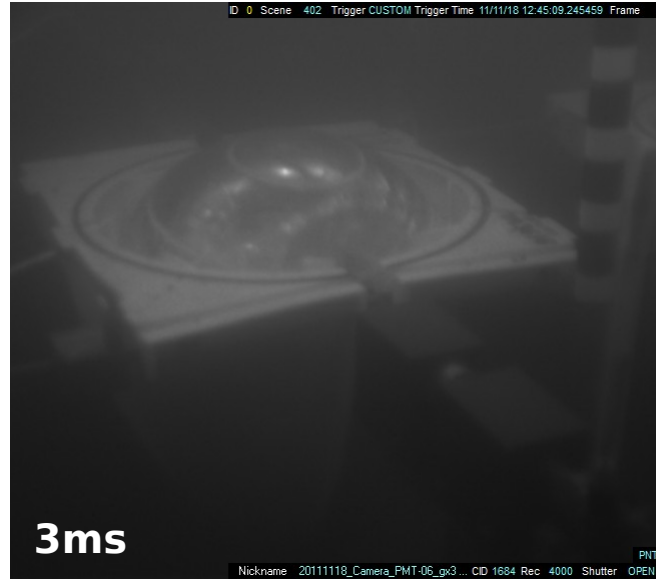
Bucket shape & ribs designed to withstand temporary differential pressure (DocDB-3574)

Multiple PMTs Experimental Setup



- 5 10" Hamamatsu R7081 tubes with prototyping housing are mounted on the cables
- Tubes are separated by 50cm from center to center
- 2 High speed cameras (4000f/s and 2000f/s)
- 10 Water proof pressure sensors (PCB ICP)
- 9 accelerometers are installed on the cables

Camera 1 Screen Shots



Camera 2 Screen Shots



Camera 2 Screen Shots



Camera 2 Screen Shots



Camera 2 Screen Shots

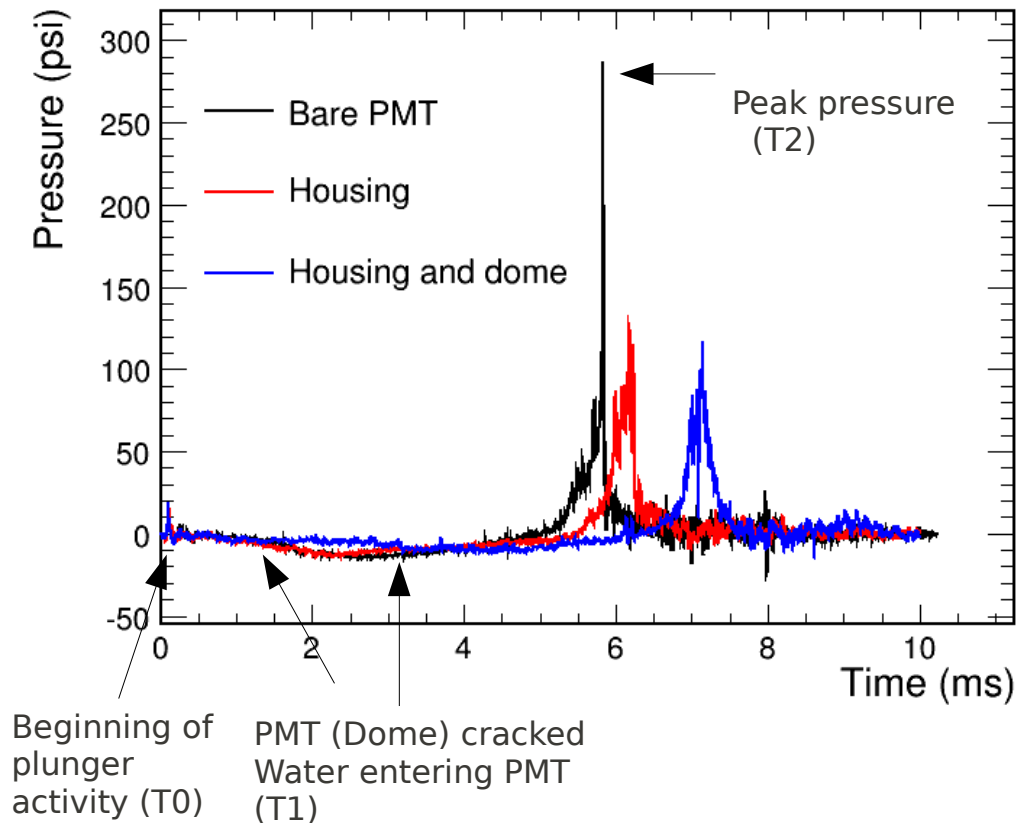


Camera 2 Screen Shots

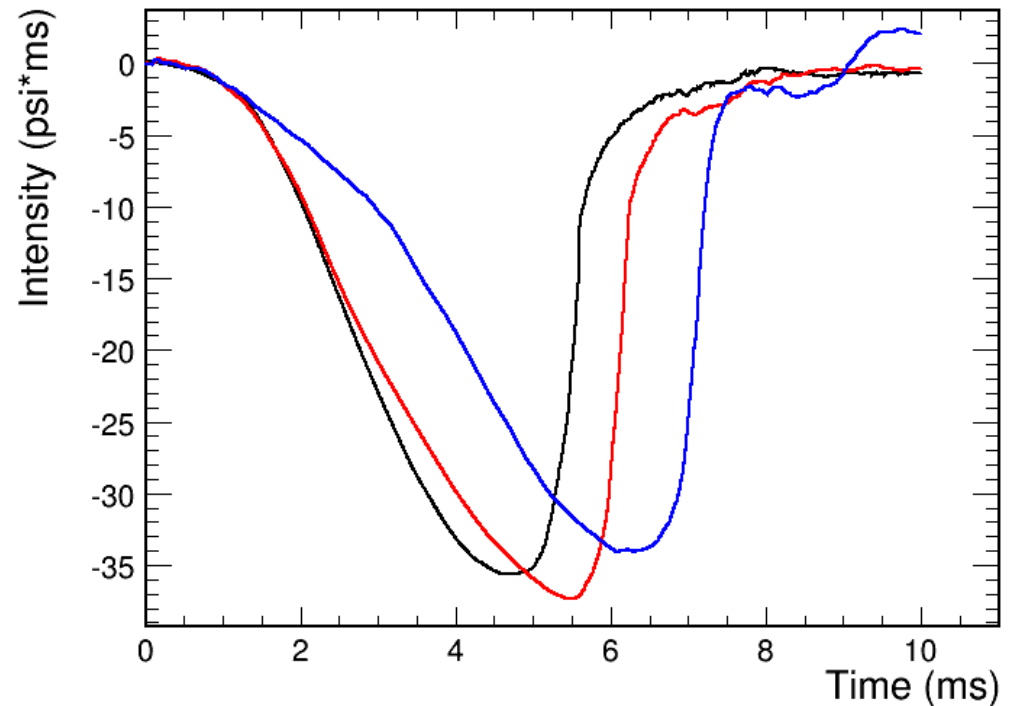


Blast Sensor Response

Blast sensor at 50cm away from implosion PMT



Blast sensor at 50cm away from implosion PMT



- The typical time scale of the pmt implosion shock wave formation is around 6ms. The dome can slow the implosion process to 7ms.
- The shock wave peak amplitudes are greatly reduced by the housing.
- The total intensity (energy) of the shock wave is consistent in all cases. Dome can slightly reduce the shock wave energy.

Housing and Dome Effect

12/16/2010 Single PMT implosion W/O bucket 10" S/N RA0249

| Sensors | distance(mm) | T0 (ms) | T2(ms) | T2-T0 (ms) | Peak (psi) | Intensity (psi*ms) |
|---------|--------------|---------|--------|------------|------------|--------------------|
| ACC11 | 152 | 0.000 | 5.570 | 5.570 | 801.6 | 150.0 |
| ACC5 | 482 | 0.260 | 5.800 | 5.540 | 300.2 | 37.8 |
| ACC1 | 521 | 0.260 | 5.785 | 5.525 | 426.9 | 38.0 |
| ACC2 | 521 | 0.245 | 5.780 | 5.540 | 488.3 | 43.2 |
| ACC3 | 521 | 0.235 | 5.830 | 5.595 | 287.2 | 35.8 |
| ACC4 | 521 | 0.245 | 5.825 | 5.580 | 410.0 | 36.3 |
| ACC6 | 991 | 0.560 | 6.150 | 5.590 | 169.2 | 20.3 |

11/16/2011 PMT implosion housing only 10" S/N TA3068

| Sensors | distance(mm) | T0 (ms) | T2(ms) | T2-T0 (ms) | Peak (psi) | Intensity (psi*ms) |
|---------|--------------|---------|---------|------------|------------|--------------------|
| S1 | 279 | 837.143 | 843.161 | 6.018 | 437.22 | 67.21 |
| S2 | 546 | 837.313 | 843.332 | 6.019 | 200.23 | 37.51 |
| S3 | 508 | 837.151 | 843.331 | 6.180 | 123.61 | 37.69 |
| S4 | 508 | 837.215 | 843.269 | 6.054 | 136.43 | 39.30 |
| S5 | 508 | 837.298 | 843.333 | 6.035 | 199.24 | 31.95 |
| S7 | 711 | 837.350 | 843.371 | 6.021 | 100.18 | 31.22 |
| S8 | 1016 | 837.653 | 843.647 | 5.994 | 107.80 | 18.59 |
| s10 | 1143 | 837.709 | 843.662 | 5.953 | 81.37 | 22.36 |

11/04/2011 Single PMT implosion with housing & dome 10" S/N ZT0007

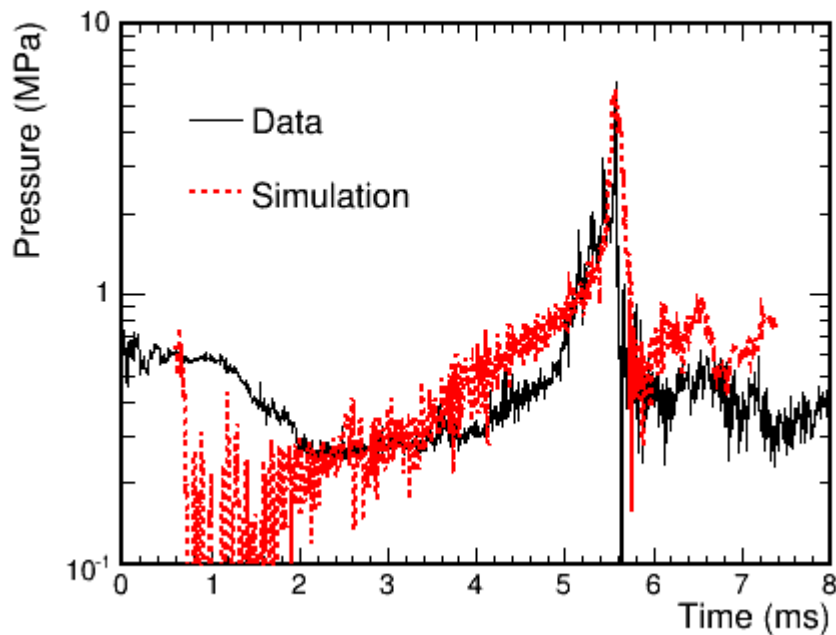
| Sensors | distance(mm) | T0 (ms) | T2(ms) | T2-T0 (ms) | Peak (psi) | Intensity (psi*ms) |
|---------|--------------|---------|---------|------------|------------|--------------------|
| S1 | 279 | 299.994 | 306.854 | 6.860 | 366.95 | 64.37 |
| S2 | 546 | 300.150 | 307.004 | 6.854 | 164.09 | 35.73 |
| S3 | 508 | 300.004 | 307.144 | 7.140 | 116.98 | 36.45 |
| S4 | 508 | 300.075 | 307.150 | 7.075 | 134.58 | 36.26 |
| S5 | 508 | 300.136 | 307.317 | 7.181 | 252.12 | 45.33 |
| S7 | 711 | 300.247 | 307.053 | 6.806 | 104.38 | 26.36 |
| S8 | 1016 | 300.493 | 307.507 | 7.014 | 101.44 | 17.15 |
| s10 | 1143 | 300.543 | 307.346 | 6.803 | 55.82 | 16.05 |

Simulation

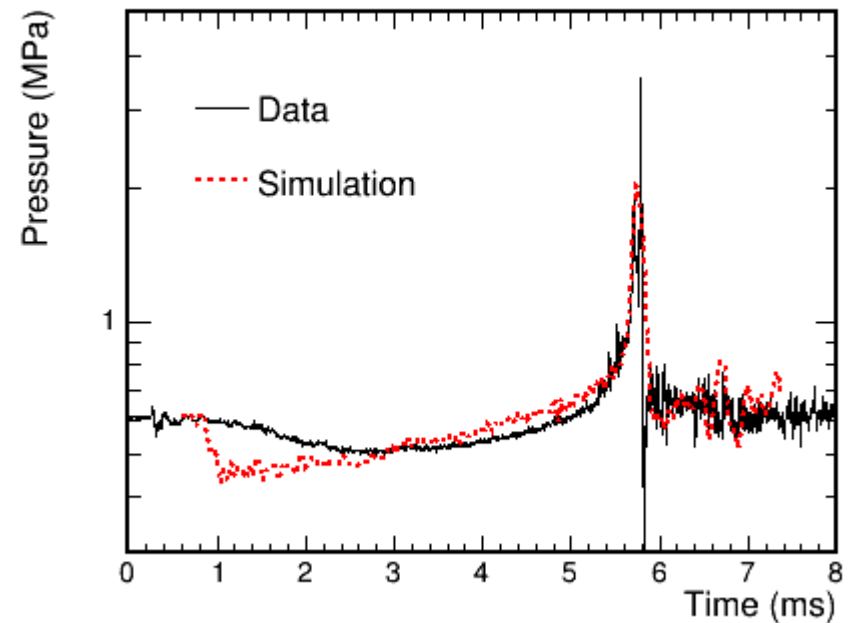
LS-DYNA (general purpose transient dynamic finite element program)
Arbitrary Eulerian-Lagrangian (ALE) formulation that allows PMT glass and fluid to interface.

Based on a 2M+ fluid/solid element model and “adjusted” PMT glass constitutive and fracture relations, the implosion at 88 psi water pressure are simulated (~240 hrs)

ACC11 Response (PMT-1)



ACC1 Response (PMT-1)



Conclusions

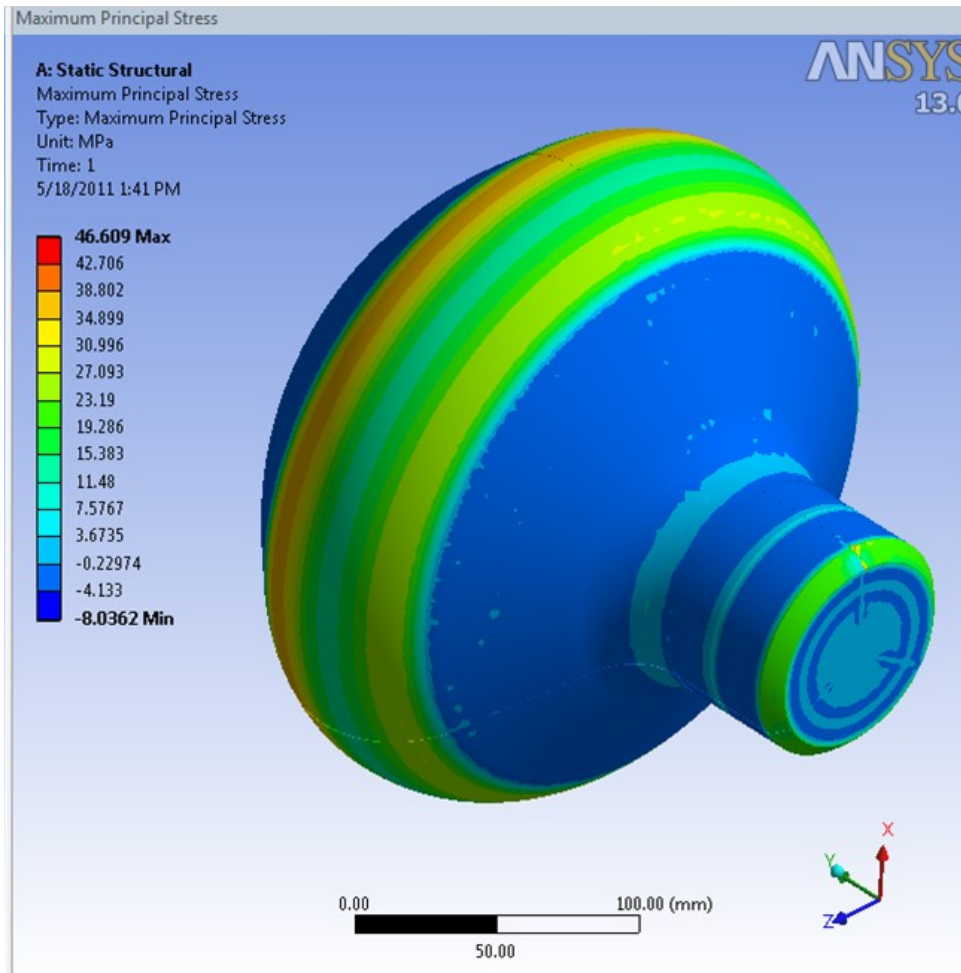
- Successfully set up slow rise pressure system at BNL.
- Multiple PMT hydrostatic pressure slow rise tests have been conducted.
- Successfully establish the PMT pressure test setup at NUWC.
- 3 identical 10" Hamamatsu PMT implosion tests with LBNE housing protection design were conducted at NUWC under 88psi. No PMT cascade implosions were found.
- The current PMT prototyping housing can effectively reduce the shock wave amplitude. The protection acrylic dome has fairly small effect on reducing the shock wave.
- PMT dynamic implosion are reasonably well simulated.

backup

Hydrostatic Stress Analysis

R. Sharma

Hydrostatic Stress Table (Hamatsu R7081)

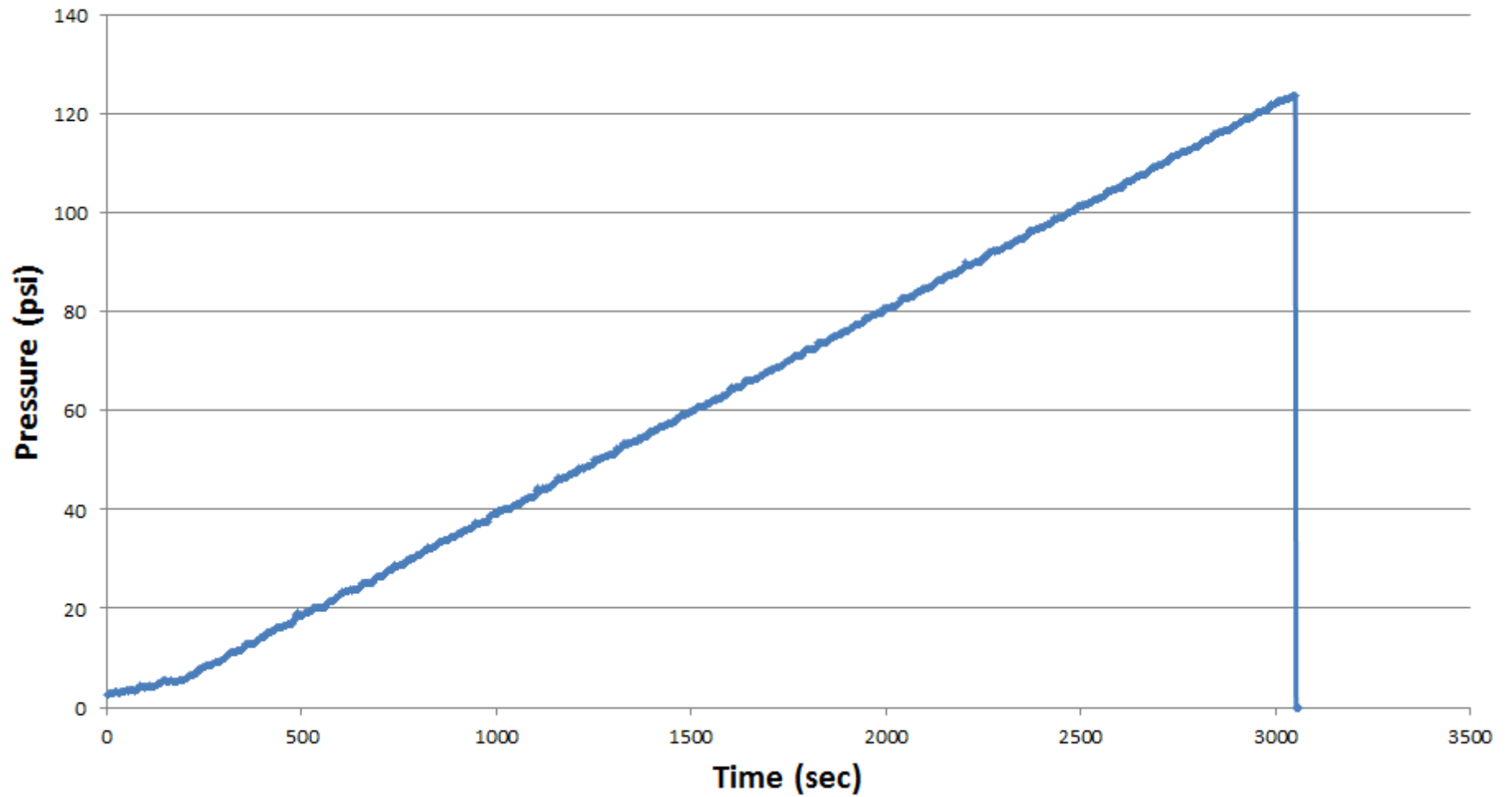


Hamamatsu R7081 under 1MPa (10 bar)

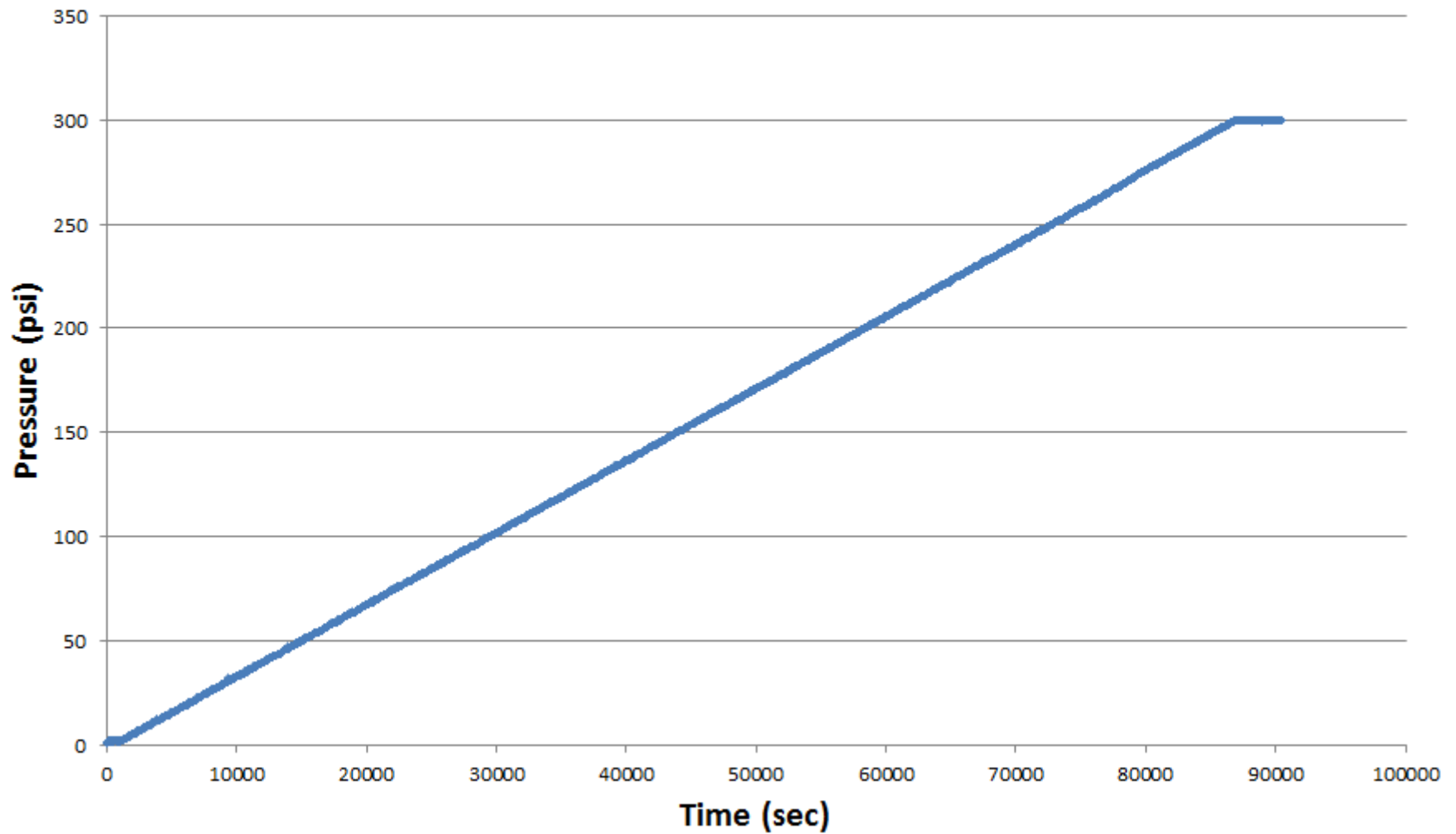
| Stress | Compressive (MPa) | Tensile (MPa) |
|--------------------------|-------------------|---------------|
| maximal principal stress | 46.6 | -8.0 |
| Maximal shear stress | 47.5 | 0.0 |
| Normal stress along X | 37.7 | -82.3 |
| Normal stress along Y | 34.6 | -68.6 |
| Normal stress along Z | 37.9 | -82.4 |
| Shear stress in XY plane | 42.7 | -44.0 |
| Shear stress in YZ plane | 42.8 | -42.6 |
| Shear stress in XZ plane | 36.9 | -37.1 |

Pressure vs. Time

2 Hour Test - 10" PMT TA3523



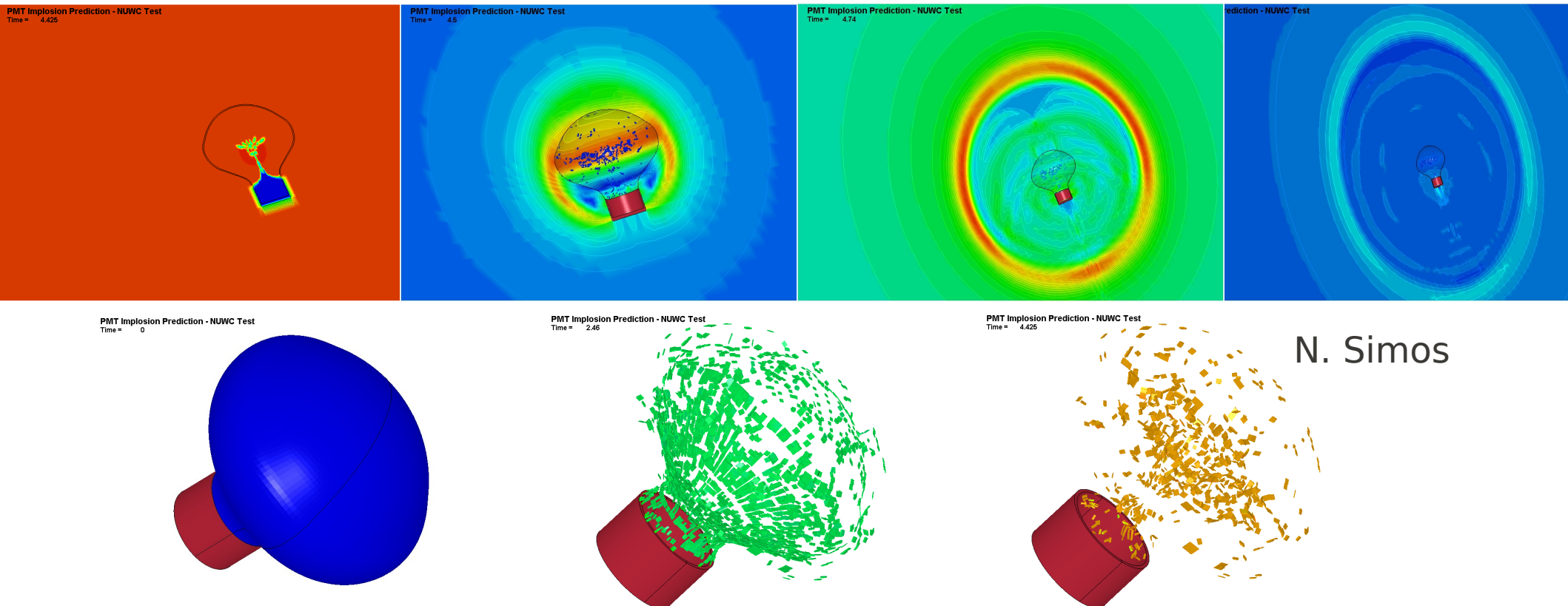
Pressure vs. Time
24 Hour Test - 12" PMT ZN0123



Simulation

LS-DYNA (general purpose transient dynamic finite element program)
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N. Simos

Electronics Shed



NUWC Control Room

